



TOTAL GW THAT COULD DISCHARGE AT START OF RECESSION, V_{tp} :

$$V_{tp} \text{ is evaluated } \int_0^{\infty} V_{tp} = \frac{Q_o t_{\log}}{2.3}$$

TOTAL GW THAT COULD DISCHARGE AT END OF RECESSION, V_R :

$$V_R \text{ is evaluated } \int_{t@end}^{\infty} V_R = \frac{Q_o t_{\log}}{2.3 \left(10^{\frac{t}{t_{\log}}} \right)}$$

1987, 1988, 1989, 1993

$Q_o \sim 150 \text{ cfs}$

$t_{\log} = \text{time for } Q \text{ to drop 1 log cycle} \sim 0.6 \text{ yr}$

$t = \text{time for recession} \sim 0.7 \text{ yr}$

$V_{tp} \sim 1.2 \times 10^9 \text{ ft}^3$

$V_R \sim 8.4 \times 10^7 \text{ ft}^3$

$V_{discharged} \sim 1.2 \times 10^9 \text{ ft}^3 \sim 26,000 \text{ AF}$



Given:

Wet Bulk Density = 2.24 g/cm³

Particle Density = 2.65 g/cm³

Fluid Density (FD) = 1.0 g/cm³

What is:

Porosity = ?

$$BD = (1 - \phi) PD + \phi (FD)$$

$$\phi = \frac{SW - DW}{V_T} \quad \frac{DW}{V_T} = PD(1 - \phi)$$

$$\phi = 1 - \frac{DW}{PD * V_T}$$

$$BD = (1 - \phi) PD + \phi (FD)$$

$$BD = PD - \phi PD + \phi FD$$

$$BD = PD + \phi (FD - PD)$$

$$BD - PD = \phi (FD - PD)$$

$$\frac{BD - PD}{(FD - PD)} = \phi$$

We have wet bulk density so $\frac{2.24 - 2.65}{1 - 2.65} = \frac{-0.41}{-1.65} \sim 0.25 = \phi$
use fluid density for water



Knowing:

Wet Bulk Density = 2.24 g/cm³

Particle Density = 2.65 g/cm³

Fluid Density (FD) = 1.0 g/cm³

Porosity = 0.25

And If:

Total Volume = 25cm³

What is:

Saturated Weight = ?

Dry Weight = ?

$$BD = (1 - \phi) PD + \phi (FD)$$

$$\phi = \frac{SW - DW}{V_T} \quad \frac{DW}{V_T} = PD(1 - \phi)$$

$$\phi = 1 - \frac{DW}{PD * V_T}$$

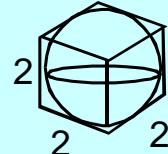
$$\text{Saturated "Weight"} = \text{Vol} * \text{WBD} = 25\text{cm}^3 * 2.24 \frac{\text{g}}{\text{cm}^3} = 56\text{g} \text{ (MASS)}$$

$$\text{Dry Weight} = \text{SatWgt} - \text{WaterWgt} = \text{SatWgt} - \phi \text{ TotVol} * \text{FD}$$

$$= 56\text{g} - (0.25 * 25\text{cm}^3) * 1 \frac{\text{g}}{\text{cm}^3} = 56\text{g} - 6.25\text{g} = 49.75\text{g} \sim 50\text{g} \text{ (MASS)}$$



$$\phi = \frac{V_v}{V_t} = \frac{2^3 - \left(m \frac{4}{3} \pi r^3 \right)}{2^3}$$



m is # spheres r is their radius

m	r	r^3	mr^3
1	1	1	1
8	1/2	1/8	1
64	1/4	1/64	1

$$\phi = \frac{2^3 - \left(\frac{4}{3} \pi \right)(1)}{2^3} = 0.476 \quad \text{A constant!}$$

HENCE MAX ϕ FOR UNIFORM, CUBIC PACKED SPHERES IS ~ 48%

MIN ϕ WOULD RESULT FROM RHOMBEHEDRAL PACKING ~ 26%

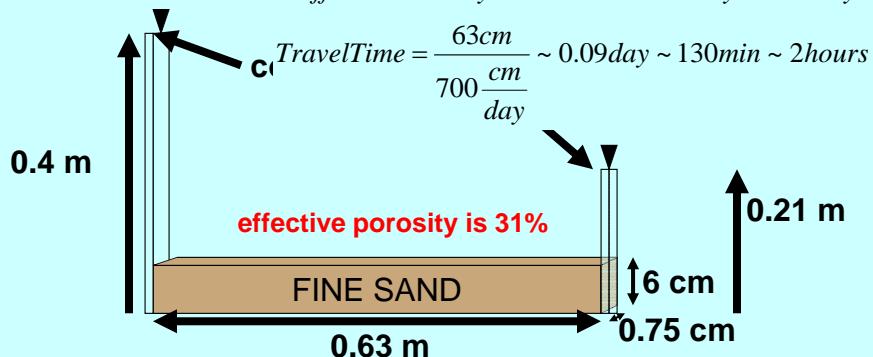
IN GENERAL, IRREGULAR PACKING & ANGULAR PARTICLES YIELD HIGHER ϕ



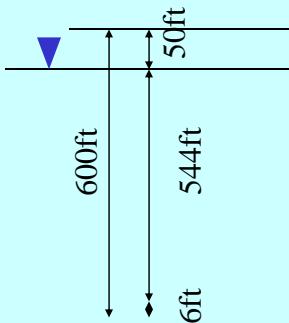
$$Q = \frac{1 \text{ liter}}{\text{day}} = \frac{1 \text{ liter}}{\text{day}} \frac{1000 \text{ cm}^3}{1 \text{ liter}} = \frac{1000 \text{ cm}^3}{\text{day}}$$

$$\text{Darcy Velocity} = \frac{Q}{\text{Area}} = \frac{\frac{1000 \text{ cm}^3}{\text{day}}}{6 \text{ cm} \times 0.75 \text{ cm}} = 222 \frac{\text{cm}}{\text{day}}$$

$$\text{Average Linear Velocity} = \frac{\text{Darcy Velocity}}{\text{Effective Porosity}} = \frac{222 \frac{\text{cm}}{\text{day}}}{0.31} = 716 \frac{\text{cm}}{\text{day}} \sim 700 \frac{\text{cm}}{\text{day}}$$



pressure on your head (6ft tall) at the bottom of a well
 surface at sea level
 bottom at 600 ft
 water level 50 ft below the surface



Gage Pressure

$$P = \gamma h = 62.4 \frac{\text{lb}}{\text{ft}^3} 544 \text{ ft} = 33945.6 \frac{\text{lb}}{\text{ft}^2}$$

$$P = 33945.6 \frac{\text{lb}}{\text{ft}^2} \frac{1}{144} \frac{\text{ft}^2}{\text{in}^2}$$

$$= 235.7 \frac{\text{lb}}{\text{in}^2} = 235.7 \text{ psi}$$

$$\text{Absolute Pressure} \sim 235.7 \text{ psi} + 14.7 \text{ psi} \\ \sim 250.4 \text{ psi}$$